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Jitter suppression in passive harmonic mode-locking fiber ring laser

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ABSTRACT

We report the results of analysis of soliton fiber ring laser with harmonic mode-locking based on the nonlinear polarization rotation and effect of gain depletion and recovery. We found that specific timing jitter connected with inequality of pulses in the cavity may occur in such type of lasers. The method of suppression of this jitter and stabilization of harmonic mode-locking operation based on the small frequency shift and filtering of laser radiation is proposed. The numerical simulations show that proposed method can provide extremely stable harmonic mode-locking for soliton fiber ring laser.

Keywords: fiber ring laser, solitons, harmonic mode-locking, jitter suppression

1. INTRODUCTION

Laser sources delivering high-repetition-rate ultrashort pulses are highly demanded in numerous photonic applications [1-6]. Among them, harmonically mode-locked (HML) soliton fiber lasers exhibiting advantageous consumer properties, such as compactness, reliability, low cost and maintaining convenient output are mostly demanded [7-9]. Some HML laser configurations comprise an intra-cavity filter, like a high-Q built-in etalon with a free spectral range (FSR) equal to the pulse repetition rate, able to select individual modes from thousands laser cavity modes to generate multi GHz sub-ps pulse trains [10, 11]. Disadvantage of this method is requirement of complex stabilization setups to synchronize the FSR of the etalon with the repetition rate of the laser [12]. Technically, the simplest way to implement HML in a ring fiber cavity is to rearrange the pulses generated through the passive mode-locking making their distribution inside the cavity strongly periodic [13-16]. Passive HML fiber lasers which are able to scale pulse repetition rates up to 20 GHz and more have been reported recently [17-19]. Timing jitter approaching to 2% of the interpulse interval and supermode suppression level (SSL) varying within a wide range from –15 dB to –60 dB and below [17–21] are considered to be typical indicators of stability of operation achieved with the HML lasers.

It is commonly accepted that a regular temporal pattern of HML formed in a fiber ring laser is induced by repulsion forces between the pulses [13, 14, 22]. However the physics of this interaction is not clear in detail. The interaction between pulses can include repulsion between antiphase pulses, interaction through saturating and relaxing dissipative parameters [23, 24] and interaction through acoustic waves induced by electrostriction [25, 26]. Besides, the role of a continuous-wave (CW) component of the optical spectrum in HML is still under discussion. It was theoretically demonstrated that a CW component acts as an efficient agent to manage the interaction between neighboring pulses. It has also been reported independently that a low power external CW does not have a major impact on the stability of the harmonic mode locking distribution, thus highlighting the robustness of an initial state HML against the external injection [27-29].

In this paper we try to emphasize the possible complexity of stable HML and assume that its stabilization is provided by a cooperative action of several mechanisms. This assumption is encouraged by the results of a report on a Tm-Ho fiber ring laser with a hybrid mode-locking combining the frequency-shifted feedback (FSF) and nonlinear polarization rotation (NPR) [20, 30]. The laser ring cavity comprises segments of active and passive SMF fibers exhibiting a total anomalous dispersion. An acousto-optic shifter with frequency shift about 40 MHz is also included into the cavity. Near the lasing threshold the laser generates subpicosecond soliton pulses with the fundamental frequency of 29.2 MHz. When the pump is increased, the laser starts to operate in HML regime demonstrating effective suppression of the supermode noise. The results of laser operation at the repetition rate of 409.4 MHz (14th harmonic of the cavity) and with SSL below -66 dB are shown in Fig. 1 (a) [20]. With an increase in the cavity length and decrease of the fundamental frequency down to 12.4 MHz, a stable HML operation is maintained. For laser operating at 1 GHz (81st harmonic of

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the longer cavity) the SSL is about -60 dB (Fig. 1 (b)).

2. HARMONIC MODE-LOCKING OBTAINED THROUGH GAIN DEPLETION AND RECOVERY

Further, we explore and describe the physical mechanism responsible for extremely stable operation in the HML lasers. The fact that a stable HML regime in [20] is available for a wide range of repetition rates and cavity lengths excludes consideration of transverse acoustic wave excitation mechanism as a mechanism responsible for laser stabilization [31]. The mechanism of HML stabilization associated with a separate CW component is also excluded due to the absence of this component in the laser optical spectrum. As a result, repulsion of pulses through the gain depletion and recovery (GDR) [32] remains the only mechanism responsible for pulse interaction.
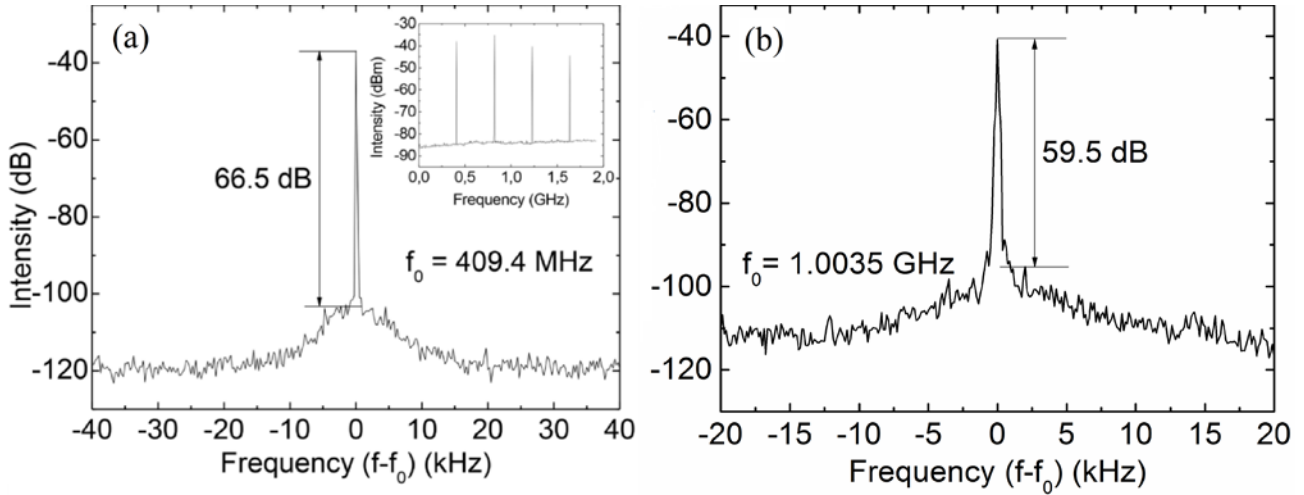

Fig. 1. RF spectrum of harmonically mode-locked Tm-Ho fiber ring laser with frequency shifted feedback. (a) The harmonic mode-locked operation showing 14th harmonic of the cavity (fundamental frequency is 29.2 MHz). Inset: The RF-spectrum with 2.0 GHz bandwidth [9]. (b) The same for the 81st harmonic of the laser with the longer cavity (fundamental frequency is 12.4 MHz).

Qualitatively, the laser gain is depleted while transferring energy to a traversing pulse. As a result, the pulse experiences a time-dependent gain, i.e. the leading edge of the pulse sees larger gain than the trailing edge (Fig. 2 (a)). The pulse with group velocity $v_g^{-1} = dt/dz$ under such condition acquires group-velocity drift towards the region of higher gain. Denoting the gain depletion during interaction with the pulse as Δg it can be shown that this group-velocity drift is proportional to the value of Δg [32].

The depletion and recovery of gain is described by the standard rate equation

$$\frac{dg_s}{dt} = \frac{g_{s0} - g_s}{\tau_g} - \frac{g_s |A(z,t)|^2}{E_g}. \tag{1}$$

Here, g_{s0} is the unsaturated gain, E_g is the gain saturation energy. Assuming that the energy E_s of the pulse is low compared to the value of E_g, gain depletion can be expressed as $\Delta g = g_s E_s / E_g$, where g_s corresponds to the value of the gain just before arriving of the pulse. If the laser cavity contains several pulses, then the GDR effect leads to their mutual repulsion. Let us analyze this interaction in more detail. For simplicity, we consider a case of two pulses. However, generalization for an arbitrary number of pulses could be also implemented. The used terms are illustrated in Fig. 2 (b). A change of the time intervals between pulses is proportional to the difference in the group-velocity drifts

$$\frac{d(T_1 - T_2)}{dz} = \Delta g_1 - \Delta g_2. \tag{2}$$

At the same time, in linear approximation for relaxation valid at $\mu = T_R/\tau_g \ll 1$ the gain depletions and interpulse distances are connected by the next equations

$$\frac{E_g}{E_{s\,3-i}}\Delta g_{3-i} - \frac{E_g}{E_{s\,i}}\Delta g_i + \Delta g_i = \mu T_i, \quad i = 1, 2.$$ (3)

Assuming that the pulse energies E_{si} are equal for all pulses, Eqs. (2) and (3) yield
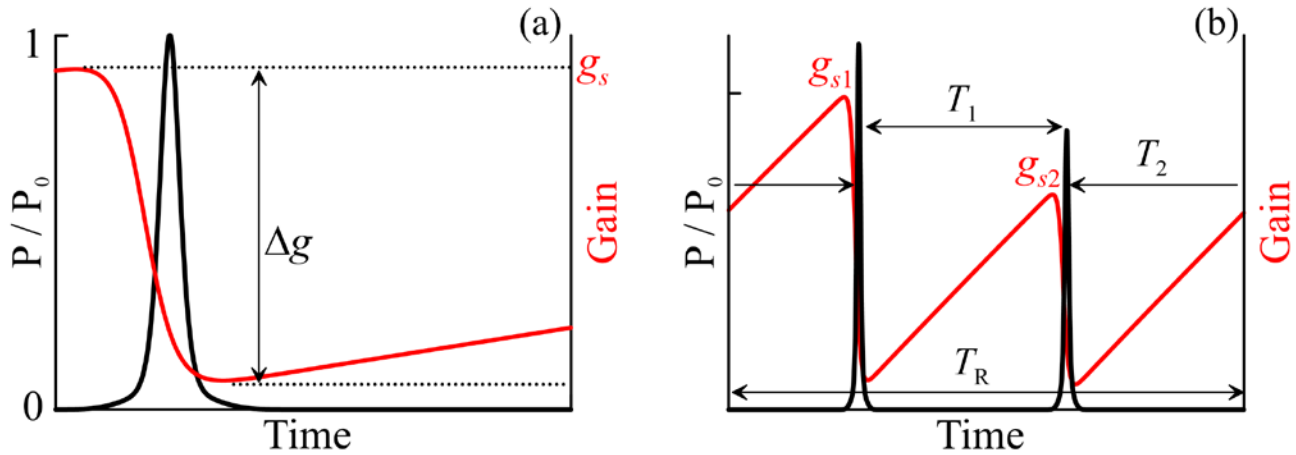

Fig.2. (a) The scheme of time-dependent gain across amplified soliton pulse. (b) The scheme of interaction through GDR in the cavity with a period $T_R = T_1 + T_2$ (T_1, T_2 are the time intervals between the pulses).

$$\frac{d(T_1 - T_2)}{dz} = -\frac{\mu}{2E_g/E_s - 1}(T_1 - T_2) = -\alpha(T_1 - T_2), \quad \alpha > 0.$$ (4)

Thus, the initial difference of time intervals tends to 0 exponentially: $(T_1 - T_2) = (T_1 - T_2)_0 \exp(-\alpha z)$, ensuring an equidistant pulse arrangement inside the cavity. This arrangement is stable since any fluctuation of $|T_1 - T_2| > 0$ decreases with the same decrement α. However, a deeper analysis shows that the higher integral gain $\int_0^L g_{si}(z)\,dz$ corresponds to the higher pulse energy E_{si} (Fig 2 (b)). So, the assumption about equality of the pulse energies is not precisely true, and pulse train possesses intensity jitter. Denoting the difference of the pulse energies as $E_{s1} - E_{s2} = \Delta(z) > 0$, Eq. (4) describing evolution of the interpulse distances can be expressed as

$$\frac{d(T_1 - T_2)}{dz} = -\alpha(T_1 - T_2) - \frac{\mu}{2E_g}\Delta(z)T_2(z).$$ (5)

In this case, the equidistant pulse arrangement $T_1 = T_2$ no longer corresponds to the stationary point of Eq. (5). Assuming that $\Delta/E_g \ll 1$ is a small random variable, we obtain that the uniform pulse arrangement due to GDR is accompanied by random changes in the interpulse distances referred to as the timing jitter of a pulse train. There are several sources of timing jitter in mode-locked lasers: pump power fluctuations, various thermal effects, and noise of the laser gain medium. HML fiber laser has an additional source of the timing jitter owing to the uncontrollable changes of adjacent pulse temporal positions, and hence this jitter is significantly stronger than the jitter in lasers operating the fundamental frequency [31]. The case described by Eq.(5) exactly belongs to this type of timing jitter specific for HML lasers. We will consider the means of suppression this jitter providing stability to the pulse train comparable with the laser operating fundamental frequency.

3. HARMONIC MODE-LOCKING STABILIZATION

Obviously, the simplest way to suppress the jitter is to eliminate the pulse energy difference Δ. For this the method of sliding-frequency filters proposed for soliton transmission lines [33-36] could be used. However in considered case this mechanism is used to stabilize the hybrid mode-locking scheme. Its action is based on the fact that soliton pulses of different energies also differ in group velocities and frequencies. Let us explain this process, following the scheme depicted in Fig. 3. We consider the case when the solitons are almost periodically arranged along the cavity
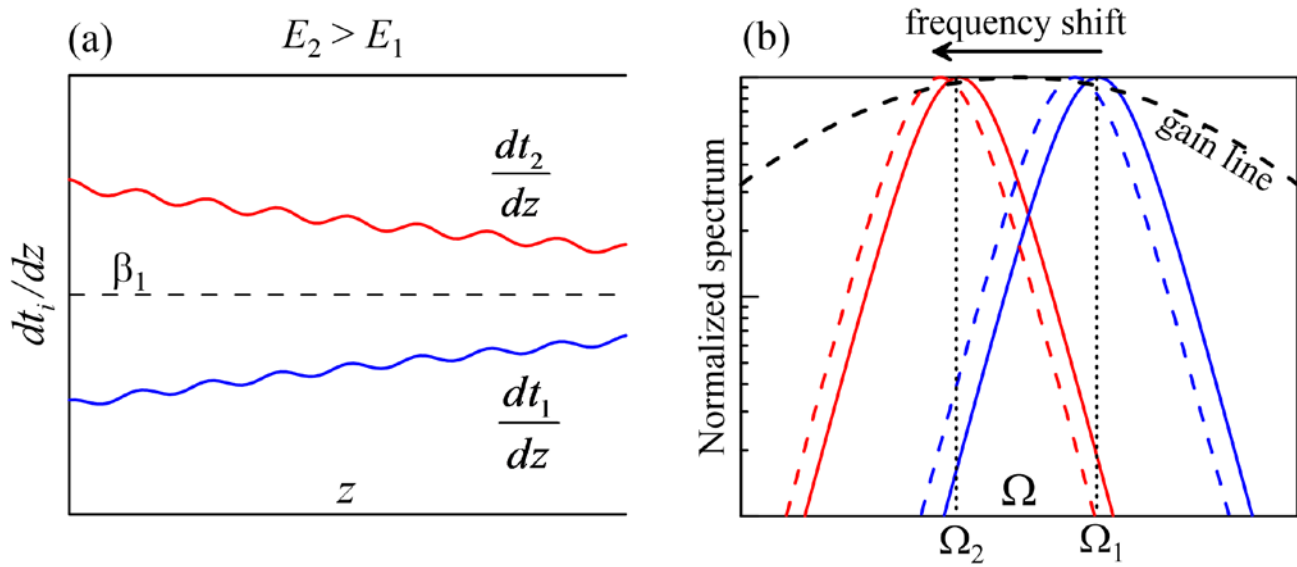

Fig. 3. (a) Change in the velocities dt_i/dz of solitons with different energies. (b) Equalization of soliton energies using frequency shift.

$T_1 \approx T_2$. Wherein, the difference in velocities dt_i/dz is mainly determined by the difference in soliton energies E_{si} (providing the velocity drift $\propto g_s E_s/E_g$). An example of change in the soliton velocities is shown in Fig. 3 (a). Here, the energy of the second soliton is higher than that of the first soliton $E_2(z) > E_1(z)$ along the whole segment z. Using the Taylor expansion, the soliton velocities can be expressed in terms of the total average velocity $(\bar{v})^{-1} = \beta_1$ and soliton frequencies:

$$dt_i/dz \approx \beta_1 + \beta_2\left(\omega_i(z) - \omega_0\right) = \beta_1 + \beta_2\Omega_i(z)$$

where ω_0 is the carrier frequency, ω_i, Ω_i are the pulse frequencies. Hence, at anomalous group velocity dispersion (GVD) $\beta_2 < 0$ a soliton of higher energy has a lower frequency and vice versa (Fig 3 (b)).

To equalize energies, the FSF method employs the spectral filtering effect. In general, a special filter can be used for this, but we consider the model case of spectrally limited gain. Fig. 3 (b) shows that at a leftward frequency shift $\Omega' = \Omega + 2\pi f$, $f < 0$, the lower frequency pulse experiences the gain less than the pulse with frequency $\Omega_1 > \Omega_2$. As a result, the pulse energies and, consequently, the pulse velocities and frequencies are equalized. This mechanism is stable and selective, i.e. the pulse with the lower energy always acquires the higher gain. When one pulse acquires higher energy than the other, its velocity dt_i/dz increases, and its frequency shifts leftward from the gain peak to an energetically unfavorable frequency domain. Noteworthy, the rightward frequency shift $f > 0$ has an opposite effect. Higher energy solitons acquire higher gain, while lower energy pulses gradually degenerate. As a result, the harmonic arrangement of pulses over the cavity is destroyed. The proposed model is applicable to the cases when there is only one mechanism associated with GDR is responsible for HML establishment. The effectiveness of this mechanism is determined by the ratio of the gain recovery timescale to the interpulse spacing and it decreases with increasing pulse repetition rate. Thus, at high repetition rate (> 10 GHz), the proposed mechanism is effective only for pulses of sufficiently high energy depleting the gain significantly.

4. NUMERICAL SIMULATION

To verify this mechanism the numerical simulation of soliton ring fiber laser with gain depletion and recovery was performed. The laser configuration is shown in Fig. 4.
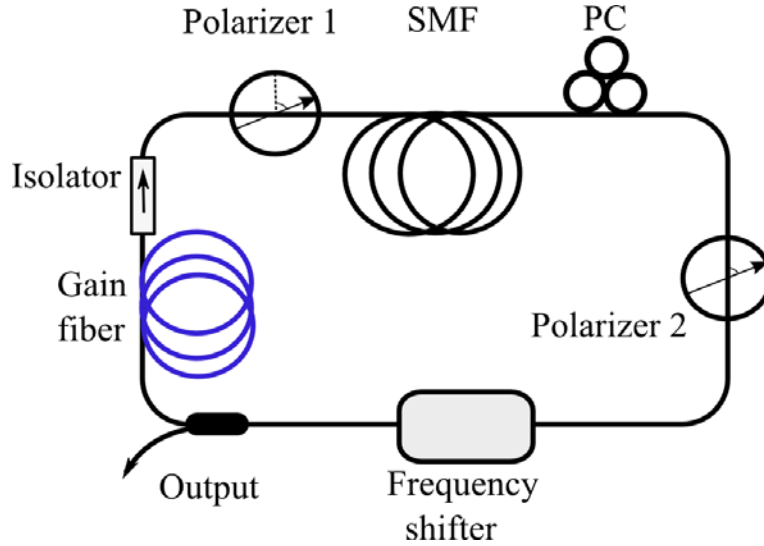

Fig. 4 Fiber ring laser configuration used in the numerical simulation.

We assume that the radiation propagating in the gain fiber is linearly polarized and it is elliptically polarized propagating in SMF. SMF has negligibly low birefringence and mode-locking effect occurs in accordance with the model [37, 38].

The field propagation in the gain fiber is described by the Ginzburg-Landau equation [39, 40]

$$\frac{\partial A}{\partial z} - i\frac{\beta_{2g}}{2}\frac{\partial^2 A}{\partial t^2} - i\gamma_g |A|^2 A = \frac{gA}{2} + \frac{\beta_{2f}}{2}\frac{\partial^2 A}{\partial t^2},$$

where z is the coordinate along the fiber, β_{2g} is the GVD and γ_g is the Kerr nonlinearity of the gain fiber. To simplify the simulation, the gain is divided into 2 parts: $g(z,t) = g_n(z) + g_s(z,t)$, $g_n \gg g_s$. The first term responsible for major contribution to the gain is time-independent. Thus, it can be averaged over the simulation window as

$$g_n(z) = g_{n0}\left(1 + \frac{1}{E_g}\int_0^{\tau_{win}} |A(z,t)|^2 \, dt\right)^{-1}.$$

where E_g is the gain saturation energy and τ_{win} is the size of simulation window. The second part corresponds to GDR and it is described by Eq.(1). The gain spectral filtering is employed in parabolic approximation $\beta_{2f} = (g_n - \overline{g}_s)/\Omega_g^2 \approx g_n/\Omega_g^2$, where Ω_g is HWFM gain line bandwidth and overbar indicates averaging over the simulation window. The light propagation in the SMF is described by two coupled nonlinear Schrödinger equations:

$$\frac{\partial A_j}{\partial z} - i\frac{\beta_2}{2}\frac{\partial^2 A_j}{\partial t^2} - i\gamma\left(|A_j|^2 + \frac{2}{3}|A_{3-j}|^2\right)A_j - \frac{i}{3}\gamma A_j^* A_{3-j}^2 = 0, \ j=1,2,$$

where β_2 is the GVD and γ is the Kerr nonlinearity coefficient in SMF. The amplitudes A_j are determined by Polarizer 1 as $A_1 = A\cos\varphi_1$, $A_2 = A\sin\varphi_1$, the polarization controller (PC) tunes the polarization angle as $A_2 = A_2\exp i\theta$ and Polarizer 2 restores the original state of polarization $A = A_1\cos\varphi_2 + A_2\sin\varphi_2$. Fiber lengths are $l_g = 2.5$ m for the gain fiber and $l_{SMF} = 5$ m for the SMF. The periodic boundary conditions are applied, i.e. the simulation window corresponds to the cavity period $\tau_{win} = T_R = T_1 + T_2$. Frequency shifter and output coupler are accounted in the transfer functions $A'(\Omega) = A(\Omega - 2\pi f)$ and $T_c \equiv A'/A = 0.95$. The frequency shift

corresponds to the step of the frequency grid $2\pi f = 1/T_R$. The main parameters of the model are listed in Table 1 [41]. We should note that the values of τ_g and T_R corresponding to real lasers are in thousands times more but to accelerate the simulation process, these values are chosen sufficiently small. They fully satisfy the necessary condition $T_R \ll \tau_g$ and the simulation provides an adequate description of the pulse interaction in the cavity. Two identical pulses exhibiting a small deviation from the equidistant arrangement $|T_1 - T_2| = 1$ ps are chosen as initial conditions. Simulation results are shown in Fig. 5. Note, a cyclic shift of the simulation window has been periodically applied.

Table 1. Parameters of the simulation.

Parameter	Value	Parameter	Value
γ , γ_g (W^{-1} m^{-1})	0.0033	E_g (pJ)	30
β_2 , β_{2g} (ps^{2}m^{-1})	-0.018	T_R (ps)	19.2
Ω_g (ps^{-1})	0.3	τ_g (ps)	300
g_{n0} (m^{-1})	1.5	g_{s0} (m^{-1})	0.1
φ_1 , φ_2	$\pi/8, \pi/2$	θ	$3\pi/4 - 0.25$

First, we consider the model that does not use the frequency shifter (Fig. 5(a-c)). The simulation results show that the conditions for amplification of pulses are not completely equivalent. Initially, the same pulses acquire unequal energies with the difference of about 0.5 pJ due to difference in the GDR values. Then, during the interaction the interpulse distances are equalized and the value of Δ decreases. However, after 10^4 round-trips it is about 1% of the single pulse energy. Finally, in the system without frequency shifter the pulse interaction through the GDR leads to the pulse arrangement in the cavity that differs from the HML equidistant distribution by significant timing jitter $|T_2 - T_1| \approx 0.25$ ps, which is more than 2.5% of the interpulse distance. The frequency shifter included into the system (Fig. 5 (d-f)) allows reducing the pulse energy difference down to nearly 0 for 1000 round-trips, thereby leading to total suppression of the timing jitter $T_2 = T_1 = T_R/2$ and stable harmonic mode-locking.
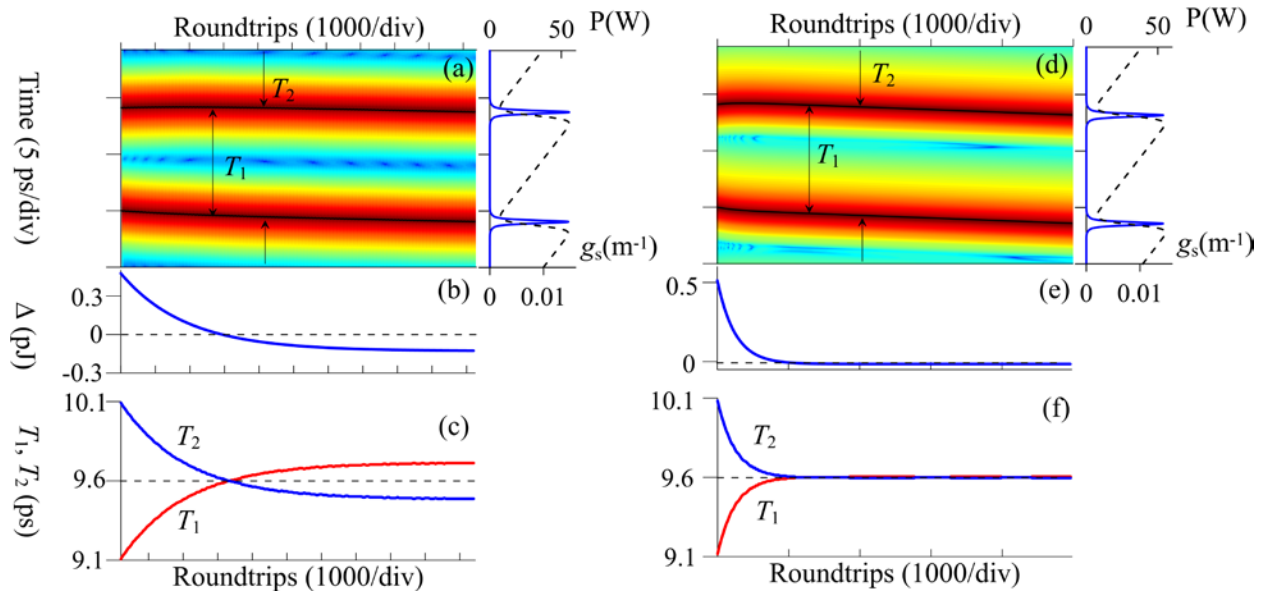

Fig. 5. (a-c) Simulation without the frequency shifter. (a) Evolution of the pulse arrangement inside the cavity. Right: the final arrangement of the pulses and GDR distribution. (b) Change of the pulse energy difference. (c) Evolution of the interpulse distances. (d-f). The same as in (a-c) but with the frequency shifter.

As mentioned above, the considered HML stabilization method can be referred to the so-called hybrid mode-locking combining the FSF and NPR techniques. Importantly, in the proposed configuration the pulse mode-locking occurs due

to the NPR mechanism alone. The role of FSF is a non-destructive pulse perturbation, leading only to the small frequency shift inside the spectral filter. In the proposed model, any small frequency shift leads to stabilization of the equidistant pulse arrangement achieved through GDR. The shift increase leads to a faster stabilization dynamics. However, it is worth noting that a system with the fixed parameters and given initial conditions is characterized by a certain threshold shift value providing HML stabilization. Exceeding this threshold value can break the dissipative balance and decrease the number of pulses. The proposed scheme of timing jitter suppression for a system with the GDR can be generalized for an arbitrary number of soliton pulses since the dependence of the pulse frequency on its energy is extended to this case as well.

5. CONCLUSIONS

In conclusion, in this paper, the soliton fiber ring laser with the passive HML has been considered. Here, the gain depletion and recovery is proposed as the pulse interaction mechanism ensuring a uniform distribution of the pulses inside the cavity. It is shown that the HML associated with such a mechanism causes the loss of identity of the pulses in the train, thus provoking timing jitter. To suppress the jitter, we propose a method to stabilize HML operation employing a small frequency shift followed by the spectral filtering.

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